

What is PV thinking?

- Two main approaches to solving fluid flow problems:
 1. We can integrate the momentum, continuity and thermodynamic equations (**the primitive equations**) directly.
 2. In certain cases we can use the vorticity – streamfunction formulation
- Often (2) is more insightful than (1).
- The vorticity – streamfunction approach can provide a neat conceptual framework in which to **understand** the dynamics.
- In certain circumstances the approach can be generalized.

How can PV thinking help the forecaster?

- **Davies and Emanuel (1991)**
 - ❖ “... a proper integration of the equations of motion is not synonymous with a conceptual grasp of the phenomena being predicted”
- **Answer**
 - ❖ “PV thinking” can provide the forecaster with a sound conceptual framework in which to interpret numerical analyses and prognoses.

Vorticity – Streamfunction method

Assumptions: homogeneous, two-dimensional, inviscid, non-rotating flow.

conservation

$$\frac{D\zeta}{Dt} = 0$$

1

vorticity

$$\zeta = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}$$

material derivative

$$\frac{D}{DT} \equiv \frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla$$

continuity

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$



$$u = -\frac{\partial \psi}{\partial y} \quad v = \frac{\partial \psi}{\partial x}$$

invertibility

$$\nabla^2 \psi = \zeta$$

2

Rotating flow on a β -plane

Assumptions: homogeneous, two-dimensional, inviscid, rotating flow on a β -plane.

conservation

$$\frac{Dq}{Dt} = 0$$

1

absolute vorticity

$$q = \zeta + f$$

continuity

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$



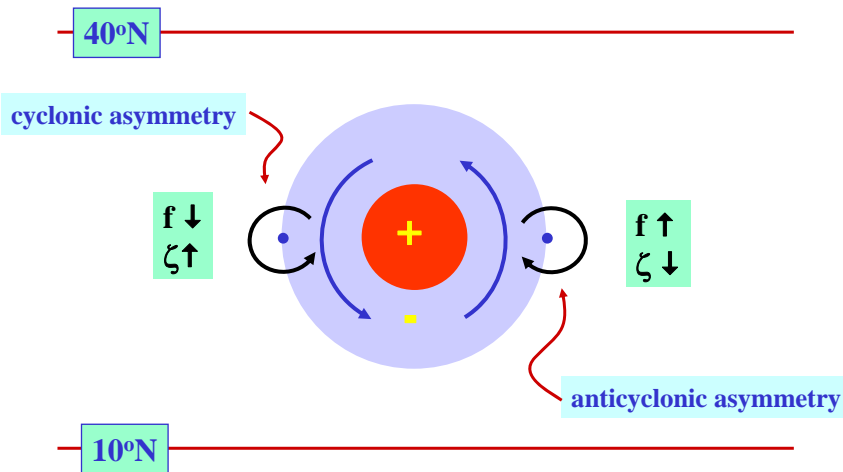
$$u = -\frac{\partial \psi}{\partial y} \quad v = \frac{\partial \psi}{\partial x}$$

invertibility

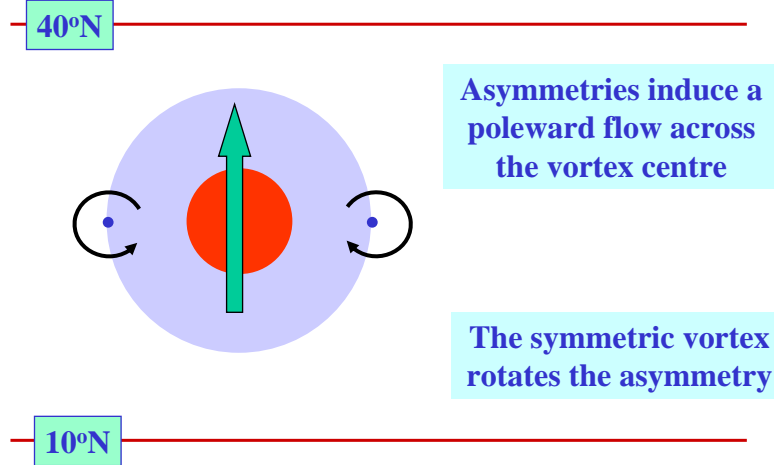
$$\nabla^2 \psi = \zeta$$

2

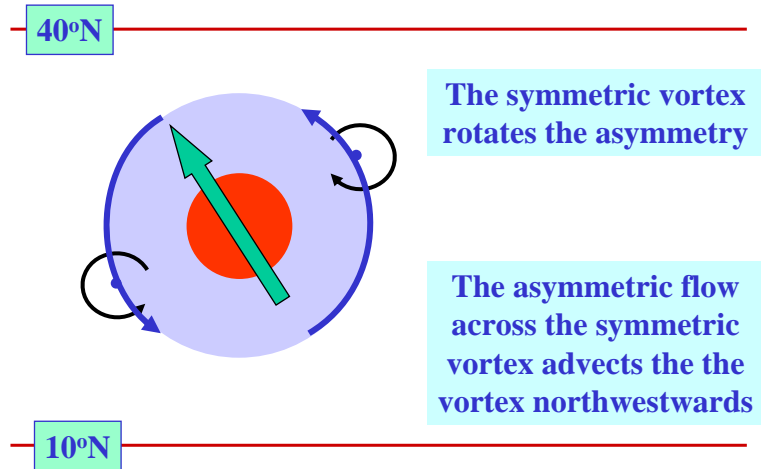
Tropical cyclone thought experiment



Tropical cyclone thought experiment

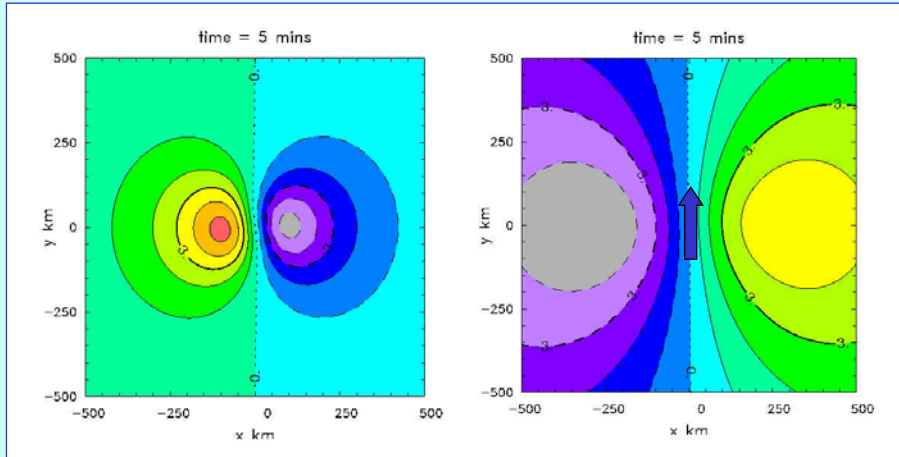


Tropical cyclone thought experiment



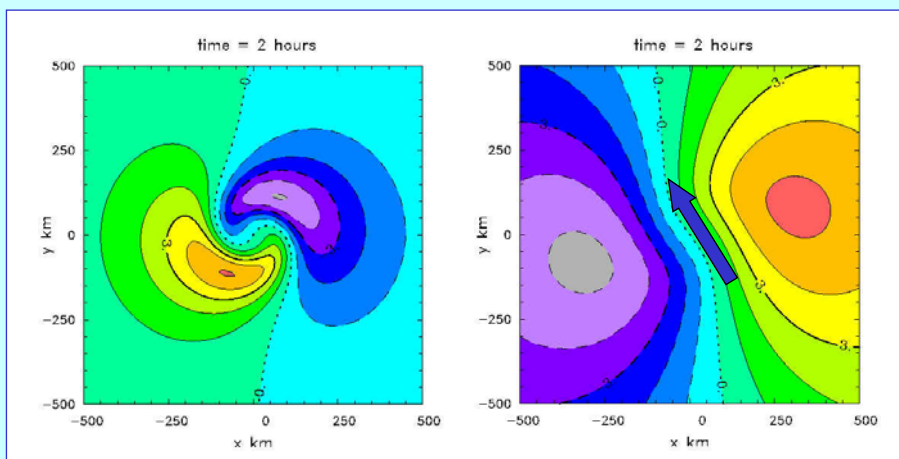
Relative vorticity

Streamfunction



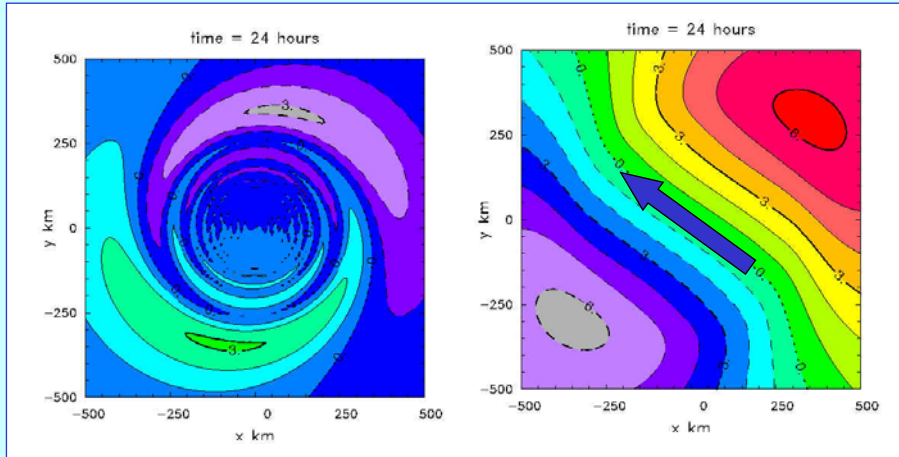
Relative vorticity

Streamfunction



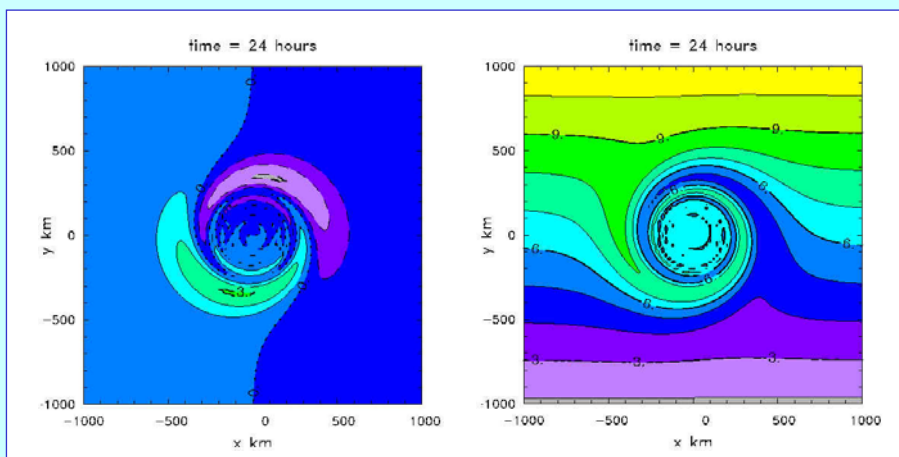
Relative vorticity

Streamfunction



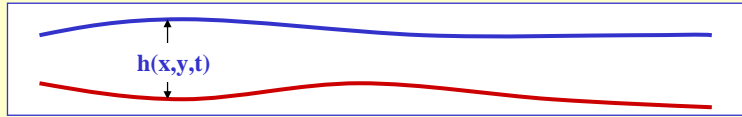
Relative vorticity

Absolute vorticity



Divergent flow, variable depth

Assumptions: homogeneous, divergent, inviscid, variable depth $h(x,y,t)$.



Conservation

$$\frac{Dq}{Dt} = 0$$

1

absolute vorticity

$$q = \frac{\zeta + f}{h}$$

continuity

$$\frac{Dh}{Dt} = -h \nabla \cdot \mathbf{u}$$

No invertibility!

Except for QG-flow

Quasi-geostrophic motion

Assumptions: stratified (Boussinesq), rotating, three-dimensional, adiabatic, inviscid, flow.

Conservation

$$\frac{Dq}{Dt} = 0$$

1

potential vorticity

$$q = \zeta + f + \varepsilon \frac{\partial^2 \psi}{\partial z^2}$$

material derivative

$$\frac{D}{DT} \equiv \frac{\partial}{\partial t} + \mathbf{u}_g \cdot \nabla$$

continuity

$$\nabla \cdot \mathbf{u}_g = 0$$



$$\mathbf{u}_g = \frac{1}{\rho f_0} \mathbf{k} \wedge \nabla p = \mathbf{k} \wedge \nabla \psi$$

Invertibility

$$\nabla_h^2 \psi + f + \varepsilon \frac{\partial^2 \psi}{\partial z^2} = q$$

2

$$\varepsilon = \frac{f^2}{N^2}$$

General adiabatic motion of a rotating stratified fluid

Assumptions: compressible, stratified, rotating, three-dimensional, adiabatic, inviscid, flow.

Conservation

$$\frac{DP}{Dt} = 0$$

1

Ertel potential vorticity

$$P = \frac{1}{\rho} (\boldsymbol{\omega} + \mathbf{f}) \cdot \nabla \theta$$

material derivative

$$\frac{D}{DT} \equiv \frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla$$

continuity

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0$$

No invertibility!

unless ...flow balanced

Isentropic coordinates

Assumptions: compressible, stratified, rotating, three-dimensional, adiabatic, inviscid, flow.

Conservation

$$\frac{DP}{Dt} = 0$$

Ertel potential vorticity

$$P = -g(\zeta + f) \frac{\partial \theta}{\partial p} = \frac{1}{\rho} (\zeta + f) \frac{\partial \theta}{\partial z}$$

material derivative

$$\frac{D}{DT} \equiv \frac{\partial}{\partial t} + u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y}$$

Formulation of an invertibility principle

- To formulate an invertibility principle one must:
- Specify some kind of balance condition, the simplest, but least accurate option being ordinary quasi-geostrophic balance,
 - Specify some sort of reference state, expressing the mass distribution of θ , and
 - Solve the inversion principle **globally**, with proper attention to boundary conditions.

Diabatic and frictional effects

PV is no longer materially conserved:

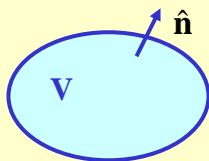
$$\begin{aligned} \frac{DP}{Dt} &= \frac{1}{\rho} \zeta_a \cdot \nabla \dot{\theta} + \frac{1}{\rho} \mathbf{K} \cdot \nabla \theta \\ &= -\frac{1}{\rho} \nabla \cdot \mathbf{Y} \end{aligned}$$

$\zeta_a =$ absolute vorticity

$\dot{\theta} =$ absolute vorticity

$\mathbf{K} = \nabla \wedge \mathbf{F}$

$\mathbf{Y} = -\dot{\theta} \zeta_a + \nabla \theta \wedge \mathbf{K}$



$$\frac{d}{dt} \int_V \rho P dV = \int_S (\dot{\theta} \zeta_a + \theta \mathbf{K}) \cdot \hat{\mathbf{n}} dS$$

Frictionless, adiabatic $\frac{d}{dt} \int_V \rho P dV = 0$

Physical interpretation

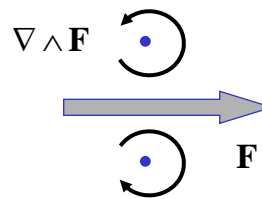
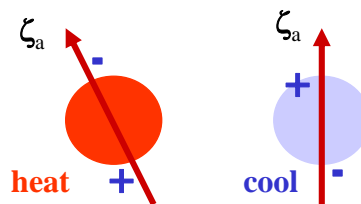
Diabatic term

$$\frac{1}{\rho} \zeta_a \cdot \nabla \dot{\theta}$$

Friction term

$$\frac{1}{\rho} \mathbf{K} \cdot \nabla \theta$$

$$\mathbf{K} = \nabla \wedge \mathbf{F}$$



Example

- Consider the case of an axisymmetric vortex with tangential velocity distribution $v(r)$.
- Assume that a linear frictional force $\mathbf{F} = -\mu v(r)$ acts at the ground $z = 0$.
- Then $\mathbf{K} = -\mu \zeta \mathbf{k}$, where ζ is the vertical component of relative vorticity.
- Then PV is destroyed at the rate

$$\frac{1}{\rho} \mathbf{K} \cdot \nabla \theta = -\frac{1}{\rho} \mu \zeta \left(\frac{\partial \theta}{\partial z} \right)_{z=0}$$